

**FATIGUE CRACK GROWTH MODEL
RANDOM2 USER MANUAL**

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**APPENDIX 1
of Annual Report
of Project Entitled
Development of Advanced Methodologies
for Probabilistic Constitutive Relationships
of Material Strength Models**

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1.0 INTRODUCTION

This User Manual documents the FORTRAN program RANDOM2. RANDOM2 is based on fracture mechanics using a probabilistic fatigue crack growth model. It predicts the random lifetime of an engine component to reach a given crack size (see Section 2.0, Theoretical Background).

Included in this Manual are details regarding the theoretical background of RANDOM2, input data instructions and a sample problem illustrating the use of RANDOM2. Appendix A gives information on the physical quantities, their symbols, FORTRAN names, and both SI and U.S. Customary units. Appendix B includes photocopies of the actual computer printout corresponding to the sample problem. Appendices C and D detail the IMSL, Ver. 10¹, subroutines and functions called by RANDOM2 and a SAS/GRAPH² program that can be used to plot both the probability density function (p.d.f.) and the cumulative distribution function (c.d.f.).

2.0 THEORETICAL BACKGROUND

Fatigue crack growth data are usually presented as cycles, N , to reach a particular crack length, a . The initial crack size is a_i . It is generally accepted that under constant amplitude alternating stress, fatigue crack growth can be related to stress intensity through a first order differential equation.³

$$da/dN = C(\Delta K)^m \quad (1)$$

where C is a material parameter, m is a material property (often a constant) and ΔK is the stress intensity range. Stress intensity range is given by

$$\Delta K = Y\Delta\sigma\sqrt{\pi a}$$

where Y is a constant dependent upon component and crack geometry and $\Delta\sigma$ is the constant amplitude alternating stress. Therefore, equation (1) can be written as

$$da/dN = C(Y\Delta\sigma\sqrt{\pi a})^m$$

or,

$$da/dN = C Y^m \Delta\sigma^m \pi^{m/2} a^{m/2} \quad (2)$$

Equation (2) can be integrated, from the initial crack length, a_i , to the final crack length, a_f , to yield N , the number of cycles. The result is

$$N = \frac{1}{CY^m \pi^{m/2} \Delta\sigma^m} \left[\frac{a_f^{-m/2+1} - a_i^{-m/2+1}}{-m/2 + 1} \right] \quad (3)$$

Thus, equation (3) gives the "cycles to reach a given crack length."

Metallurgical evidence indicates that casting pores play a significant role in the high-cycle fatigue life of cast nickel base-superalloys, especially at high temperatures.⁴ The location and size of these fatigue crack-initiating pores vary greatly from one aerospace propulsion system component to another. This accounts for the large variability in fatigue life and leads to consideration of fatigue crack growth as a random phenomenon.

Fatigue life directly relates to casting pore size, and pore size can be used to determine initial crack size, a_i . Thus, utilizing principles of both probabilistic analysis and fatigue crack growth, a quantitative probabilistic constitutive relationship between fatigue life and fracture mechanics parameters can be developed. Using the "randomized equation" approach, the fatigue crack growth model, given by equation (3) has the following form:

$$N = f(C, m, \Delta\sigma, a_i, a_f, Y) \quad (4)$$

or, in general,

$$N = f(X_i), i = 1, \dots, 6, \quad (5)$$

where the X_i are the six independent variables in equations (3) and (4). Equation (3) is "randomized" by assuming the first four variables in equation (4) to be random. Assuming a small crack in a relatively large component leads to assuming $Y = 1.0$, a deterministic value. A deterministic final crack size was chosen since experimental evidence indicated that it was relatively unimportant.³

Probabilistic analysis, via simulation, yields the distribution of the dependent random variable, cycles, N . A probability density function (p.d.f.) of cycles is generated using the maximum penalized likelihood method. Maximum penalized likelihood generates the p.d.f. estimate using the method of maximum likelihood together with a penalty function to smooth it.⁵

3.0 INPUT DATA

Data input for RANDOM2 is user friendly and easy to manipulate (see, for example, the file entitled NORMAL.INP, in Section 4.0). The first five lines of input have the same format, namely 2E12.4, and the last two lines differ. The last two lines of input have the formats I3,2X,I3,2X,2E12.4,2X,I3 and I3, respectively. A brief line by line description is given along with an example for each line (Note: the ruler is to aid the user in formatting and is not a part of the input). A table listing the physical quantities, their units and symbols is given in Appendix A.

1. Random Number Generator Seed, ISEED, and Sample Size, NTOT

EXAMPLE:

```
123456789012345678901234567890
      1                      40
```

2. Material Property, RMM

EXAMPLE:

```
123456789012345678901234567890
      28.0E-01          1.4E-01
```

3. Initial Crack Size (Pore Diameter), RAI

EXAMPLE:

```
123456789012345678901234567890
      300.0E-06        45.0E-06
```

4. Material Property, RCC

EXAMPLE:

```
123456789012345678901234567890
      2.20E-11         0.22E-11
```

5. Stress Range, DELSIG

EXAMPLE:

```
123456789012345678901234567890
      6.2E+02          6.2E+01
```

6. The DESPL¹ parameters are NODE, INIT, ALPHA, EPS, MAXIT and are entered in that order as follows:

EXAMPLE:

1234567890123456789012345678901234567890
21 0 50.0E-01 10.0E-05 30

7. The DESPL parameter, IOPT, is entered as follows:

EXAMPLE:

1234567890
2

4.0 SAMPLE PROBLEM FOR RANDOM2

The objective of this program is to predict the random lifetime, to reach a given crack size for an engine component . The theory is based on fracture mechanics, using a probabilistic fatigue crack growth model (see Section 2.0, Theoretical Background). RANDOM2 input parameters are given in Table A1.1. Note that the first four parameters are random. Their means and standard deviations are input by the user. The last two parameters, A_f and Y , are deterministic and are fixed internally by the program. They are equal to the values shown in Table A1.1.

Table A1.1 RANDOM2 sample problem input (SI units)

FORTRAN Name	Distribution Type	Mean	Standard Deviation	
			(Value)	(% of Mean)
RMM	normal	28.0E-01	1.4E-01	(5%)
AI	lognormal	300.0E-06	45.0E-06	(15%)
RCC	lognormal	2.20E-11	0.22E-11	(10%)
DELSIG	lognormal	6.2E+02	6.2E+01	(10%)
AF	N/A	2.0E-03	N/A	
YY	N/A	1.0	N/A	

The input is entered in the following format in a file entitled NORMAL.INP.

```

1234567890123456789012345678901234567890
      1              40
28.0E-01      1.4E-01
300.0E-06      45.0E-06
2.20E-11      0.22E-11
6.2E+02      6.2E+01
21      0      50.0E-01      10.0E-05      30
2

```


Execution of RANDOM2 (source code entitled NR2.FOR) produces an output file entitled RANDOM22 giving intermediate results (see Appendix B). Execution also produces the plotfiles OUT1 and OUT2 (see Appendix B). These files are used to plot the X and Y axes of the probability density function (p.d.f.) and the cumulative distribution function (c.d.f.), respectively, generated by RANDOM2. The plots are drawn from the plotfiles by the SAS/GRAPH graphing program (see Appendix C). These plots for the sample problem are shown in Figures A1.1 and A1.2.

This same sample problem has been reported in Boyce and Chamis.⁶ There, however, it utilized U.S. Customary units and an older version of RANDOM2 (IMSL Version 9.2 subroutines).

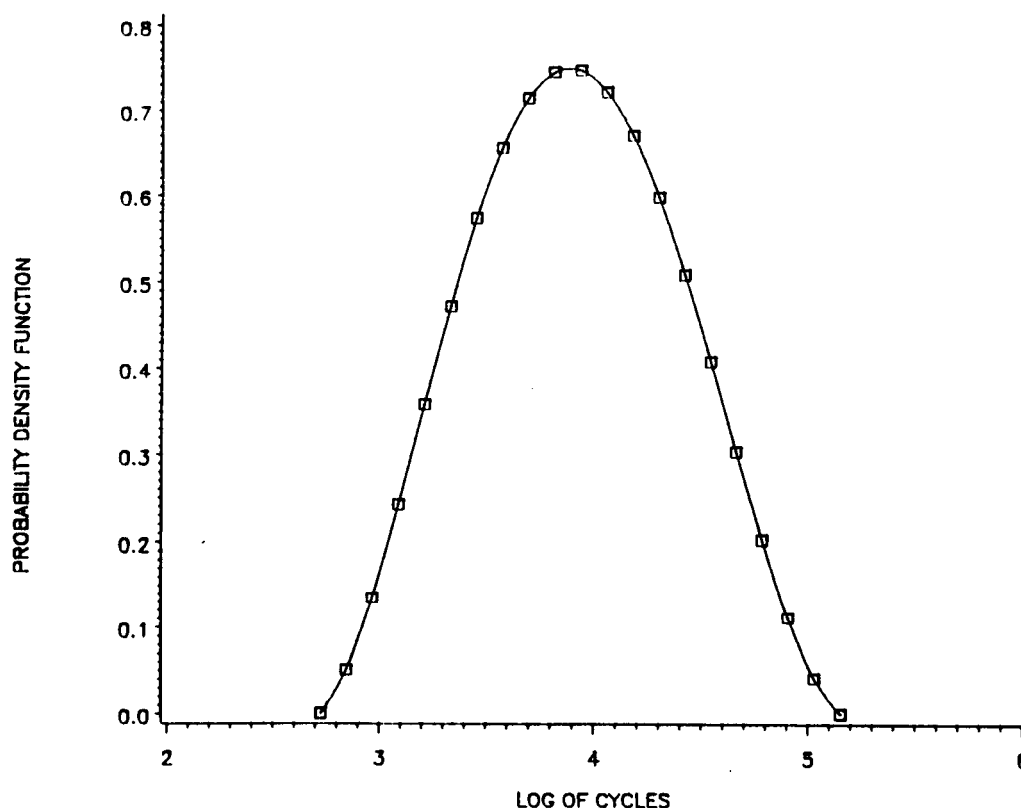


Fig. A1.1 p.d.f. of log of mechanical cycles for fatigue crack growth model, using maximum penalized likelihood.

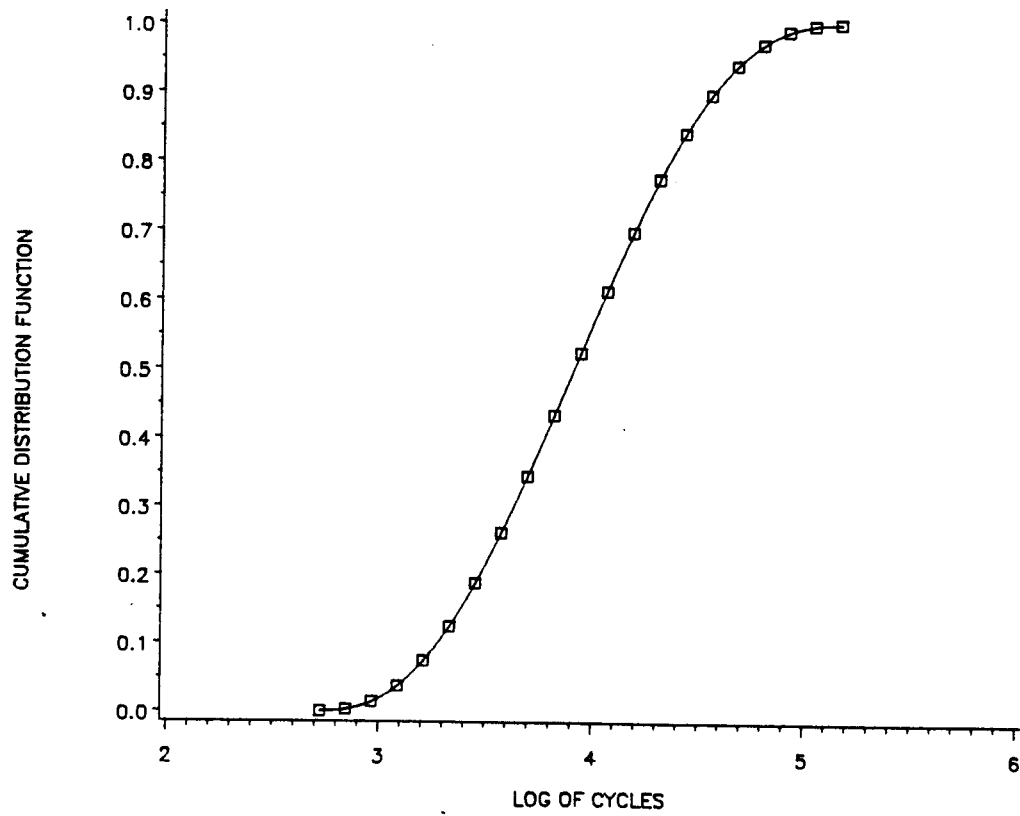


Fig. A1.2 c.d.f. of log of mechanical cycles for fatigue crack growth model, using maximum penalized likelihood.

5.0 REFERENCES

- ¹IMSL, "STAT/LIBRARY, FORTRAN Subroutines for Statistical Analysis", Houston, Texas, 1987.
- ² SAS Institute, Inc. SAS/GRAPH User's Guide, Version 5 Edition, Cary, NC: SAS Institute, Inc., 1985, p. 596.
- ³ Kozin, F. and Bogdanoff, J.K., "A Critical Analysis of Some Probabilistic Models of Fatigue Crack Growth," Engineering Fracture Mechanics, Vol. 14, 1981, pp. 55-89.
- ⁴ Hoffeler, W., "High-Cycle Fatigue-Life of the Cast Nickel Base-Superalloys in 738 LC and IN 939," Metallurgical Transactions A, Vol. 13A, July, 1982, pp. 1245-1255.
- ⁵ Scott, D.W., "Nonparametric Probability Density Estimation by Optimization Theoretic Techniques," NASA CR-147763, April, 1976.
- ⁶ Boyce, L. and Chamis, C.C., "Probabilistic Constitutive Relations for Cyclic Material Strength Models," Proceedings, 29th Structures, Structural Dynamics and Materials Conference, Williamsburg, VA, 1988.

6.0 APPENDIX A

PHYSICAL QUANTITIES, SYMBOLS, AND UNITS

The physical quantities, their symbols, and units for the fatigue crack growth model are given in the following table.

Table A1.2 Physical quantities, symbols, and units
for fatigue crack growth model for RANDOM2

Physical Quantity	Theory Symbol	FORTRAN Name	Units	
			SI	U.S.
Material Property	m	RMM	m/cycle/M Pa	m in/cycle/ksi
Initial Crack Size	A _i	RAI	m	in
Material Property	C	RCC	m/cycle	in/cycle
Alternating Stress	$\Delta\sigma$	DELSIG	M Pa	ksi
Final Crack Size	A _f	AF	m	in
Geometry Dependent Constant	Y	YY	(dimensionless)	

7.0 APPENDIX B

SAMPLE PROBLEM: SOURCE, INPUT AND OUTPUT FILES

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```
CALL RNSET(ISEED)
CALL RNML(NTOT, YM, YS, RCC)
WRITE(6, 2021)
2021 FORMAT(' MATERIAL PROPERTY, C')
C LOGNORMAL STRESS RANGE, DELSIG
WRITE(6, 1001) (RCC(I), I=1, NTOT)
WRITE(6, 1002) ISEED, NTOT
READ(5, 1011) XM, XS
WRITE(6, 1011) XM, XS
XS = 0.62E+02
XM = 6.2E+02
YS = SORT(LOG(1.0+(XS/XM)**2))
YM = LOG(XM) - 0.5*YS**2
CALL RNSET(ISEED)
CALL RNML(NTOT, YM, YS, DELSIG)
WRITE(6, 2022)
2022 FORMAT(' STRESS RANGE, DELSIG')
C DEFINE DETERMINISTIC PARAMETERS
C PI
PI = 3.1415926535897932384626433
C COMPONENT AND CRACK SHAPE PARAMETER, YY
YY = 1.0
C FINAL CRACK SIZE, AF
AF = 2.0E-03
C CALCULATE CYCLES TO REACH CRACK SIZE 2.0E-03M
DO 101 I=1, NTOT
  XNF1 = 1.0/(RCC(I)*YY**RMM(I)*PI**((RMM(I)/2.)*DELSIG(I)**
  1 RM(I)))
  XNF2 = (AF**((1.-RMM(I)/2.))-RAI(I)**(1.-RMM(I)/2.))/
  1 (1.-RMM(I)/2.)
  XNF(I) = XNF1*XNF2
C CALCULATE LOG OF CYCLES TO REACH CRACK SIZE 2.0E-03M
  XNF(I) = ALOG10(XNF(I))
101 CONTINUE
2023 FORMAT(' LOG OF CYCLES TO REACH CRACK SIZE=2.0E-03M, ', /)
1, GIVEN STRESS MEAN AMPLITUDE=6.2E+02MPA')
WRITE(6, 1001) (XNF(I), I=1, NTOT)
C SORT LOG OF CYCLES
CALL SORT(XNF, NTOT)
WRITE(6, 2024)
2024 FORMAT(' SORTED LOG OF CYCLES')
WRITE(6, 1001) (XNF(I), I=1, NTOT)
CXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
C CALCULATE PDF OF LOG OF CURRENT CYCLES, LOG XNF
READ(5, 1009) NODE, INIT, ALPHA, EPS, MAXIT
WRITE(6, 985)
985 FORMAT(' DESPL PARAMETERS')
WRITE(6, 1009) NODE, INIT, ALPHA, EPS, MAXIT
BND5(1) = XNF(1) - 0.05*XNF(1)
BND5(2) = XNF(NTOT) + 0.05*XNF(NTOT)
WRITE(6, 979) BND5(1), BND5(2)
979 FORMAT(' BND5(1), BND5(2) = ', E12.4, ' ', E12.4, ' ', /)
CALL DESPL(NTOT, XNF, NODE, BND5, INIT, ALPHA, MAXIT, EPS, DENS, STAT,
1 NMIS)
WRITE(6, 980)
980 FORMAT(' PDF OF LOG OF CURRENT CYCLES, LOG XNF, Y AXIS OF PDF PLOT')
WRITE(6, 1001) (DENS(I), I=1, NODE)
WRITE(6, 981)
981 FORMAT(' OUTPUT STATISTICS')
WRITE(6, 1001) (STAT(I), I=1, 4)
WRITE(6, 982)
982 FORMAT(' NUMBER OF MISSING VALUES')
```



```

WRITE(6,1010)NHMISS
C
C CALCULATE WINDOW WIDTH, HH
C
      HH=(BND(2)-BND(1))/(NODE-1)
C
C CALCULATE VALUES OF LOG OF CURRENT CYCLES AT WHICH PDF IS ESTIMATED;
C ALSO CALLED "NODE" VALUES
C
      DO 6001,I=1,NODE-2
        BND(I+2)=BND(I) + (I*HH)
      CONTINUE
      6001 WRITE(6,983)
      983 FORMAT(1010)LOG OF CURRENT CYCLES, LOG XNF')
      WRITE(6,1001)(BND(I),I=1,NODE)
C
C REORDER BND FOR PLOTTING
C
      SAVE1 = BND(2)
      SAVE2 = BND(NODE)
      BND(NODE)=BND(2)
      BND(2)=BND(NODE)
      DO 6002,I=1,NODE-2
        BND(I+1)=BND(I+2)
      CONTINUE
      BND(NODE-1)=SAVE1
      BND(NODE)=SAVE2
      6002 WRITE(6,984)
      984 FORMAT(1010)ORDERED LOG OF CURRENT CYCLES, LOG XNF,
      1X AXIS PDF, CDF PLOT')
C
C WRITE LOG OF CURRENT CYCLES AND PDF OF LOG OF CURRENT CYCLES,
C LOG XNF TO PLOT FILES
      WRITE(34,990)
      990 FORMAT('E12.4,I12.4')
      991 WRITE(34,991)(BND(J),J=1,NODE)
      991 FORMAT(E12.4,I12.4)
C
C CALCULATE CDF OF LOG OF CURRENT CYCLES
C
      READ(5,1010)IOPT
      WRITE(6,992)
      992 FORMAT(' GPDF PARAMETERS')
      WRITE(6,1010)IOPT
      XO=BND(1)
      DO 6003,I=1,NODE
        P=GPDF(XO,IOPT,NODE,BND,DENS)
        BNDX(I)=XO
        XO=XO+HH
      CONTINUE
      DISX(I)=P
      6003 WRITE(6,994)
      994 FORMAT(' CDF OF LOG OF CURRENT CYCLES, LOG XNF,
      1X AXIS OF PDF, CDF PLOT')
      WRITE(6,1001)(DISX(I),I=1,NODE)
C
      WRITE(6,993)
      993 FORMAT(' ORDERED LOG OF CURRENT CYCLES, LOG XNF,
      1X AXIS OF PDF, CDF PLOT')
      WRITE(6,1001)(BND(I),I=1,NODE)
      WRITE(6,1001)(BNDX(I),I=1,NODE)
C
C WRITE LOG OF CURRENT CYCLES AND CDF OF LOG OF CURRENT
C TO THE PLOT FILES

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WRITE(35,990)
WRITE(35,991)(BNDS(J),DISTX(J),J=1,NODE)
STOP
END
CXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
SUBROUTINE SORT (Y,N)
DIMENSION Y(10000)
C Y IS THE ARRAY TO BE SORTED
C AT COMPLETION Y(1) IS SMALLEST VALUE
C AT COMPLETION Y(N) IS LARGEST VALUE
N1 = N - 1
DO 1 I=1,N1
  J = I + 1
  DO 2 K=J,N
    IF (Y(I).LT.Y(K))GO TO 2
    TEMP = Y(I)
    Y(I) = Y(K)
    Y(K) = TEMP
  2 CONTINUE
  1 CONTINUE
END

```

```

-----
IMSL Name: D3SPL/DD3SPL (Single/Double Precision version)
Computer: IBM/SINGLE
Revised: November 1, 1985
Purpose: Nonparametric probability density function estimation
         estimation by the penalized likelihood method.
Usage:   CALL D3SPL (NORS, X, NODE, BNDS, INIT, ALPHA, MAXIT, EPS,
         DENS, STAT, LDHES, ILOHI, DENEST, B,
         IPUT, WK2)

```

Arguments:

- NORS - Number of observations. (Input)
- X - Vector of length NORS containing the random sample of responses. (Input)
- NODE - Number of mesh nodes for the discrete pdf estimate. (Input)
- BNDS - Vector of length 2 containing the minimum and maximum values for X(1) in BNDS(1) and BNDS(2), respectively. (Input)
- INIT - Initialization option. (Input)
- ALPHA - Positive penalty weighting factor which controls the smoothness of the estimate. (Input)
- MAXIT - Maximum number of iterations allowed in the iterative procedure. (Input)
- EPS - Convergence criterion. (Input)
- DENS - Vector of length NODE containing the estimated values of the discrete pdf at the NODE equally spaced mesh nodes. (Input/output if INIT=1, Output otherwise)
- STAT - Vector of length 4 containing out statistics. (Output) STAT(1) and STAT(2) contain the log-likelihood and the log-penalty terms, respectively. STAT(3) and STAT(4) contain the estimated mean and variance for the estimated density.
- LDHES - Seven by SEVEN hessian matrix (and its factorization). (Output)
- ILOHI - Leading dimension of HESS exactly as specified in the dimension statement in the calling program. (Input)
- BNDS - NODE by 2 matrix containing the indices for the risk set

```

DENEST - NODE by 3matrix containing the gradient vector, among
        other quantities. (Output)
B - vector of length NODE contains the NODE values.
    (Output)
INPUT - pivot vector of length NODE-2. (Output)
MK2 - work vector of length NODE-2. (Output)

```

Chapter: STAT/LIBRARY Density and Hazard Estimation

Copyright: 1985 by IMSL, Inc. All Rights Reserved.

Warrants: IMSL warrants only that IMSL testing has been applied to this code. No other warranty, expressed or implied, is applicable.

SUBROUTINE D3SPL (NORS, X, NODE, BNDS, INIT, ALPHA, MAXIT, EPS,
DENR, STAT, HESS, LDHESR, ILOHI, DENEST, B,
IPVT, WK2)

```

INTEGER
      IPVT, WKZ)
      NOBS, NODE, INIT, MAXIT, LDHES, ILOHI(NODE,*),
      IPVT(*))
      SPECIFICATIONS FOR ARGUMENTS

```

```

REAL
IPV1(*)
ALPHA, EPS, X(*), RND5(2), DENS(*), STAT(4),
HESS(LDHES,*), DENEST(NODE,*), B(*), WK2(*)

```

```

INTEGER
REAL
I, IMPTR, IPTR, ITER, K, KMI, KM2, KPI, KP2, H, H2, H3,
NEN, NOBI
BK, BKMI, BSMALL, CK, CKMI, CKM2, CKMCM1, CKP1, CKP2,
CONS, EPS1, FACTOR, FK, FKM1, FKM2, FKP1, H, H2, H3,
SUM, TEMP, WK(4)

```

```

DOUBLE PRECISION SUM1, SUM2, SUM3
INTEGER MINCR(8)
SPECIFICATIONS FOR SAVE VARIABLES

```

DERIVE INTRINSIC ALLOC,amax1,max0,min0,mod,sqrt INTEGER MAXO, MINO, MOD	SPECIFICATIONS FOR INTRINCS
---	-----------------------------

EXTERNAL	INTERNAL	FUNCTION	DESCRIPTION
INTEGER	MAXO, MINO, MOD		
REAL	ALOG, AMAX1, SORT		
			SPECIFICATIONS FOR SUBROUTINES
		FINES, FIBOS, FIBSH, FIBST, FIBTE, FIBV	

[illegible]

```
INTEGER ISMIN, NIRC0,  
REAL SDOT, SNRM2, SSUM
```

DATA MINCR/5, 9, 17, 33, 65, 129, 253, 100001/

CALL E1PSH ('D3SPL ')

NER = 1

Error checks

```
IF (NROWS - LJ) THEN
  CALL EIMES
  (5, 1, 'After removing all missing (NaN, not a
  (number) values from X there are no valid
  ,observations'. At least one valid observation
  ,is necessary.')
```

```

END IF
IF (NODE.LE. 4) THEN
  CALL E1ST(1, NODE)
  CALL E1MS(5, 2, NODE = % (I1), 'nodes, NODE, must be an odd integer greater
  'is necessary. ')
  'The number of mesh '
  '
  '

```

```

nodes, NUDE, must be an odd integer greater //

```

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1000      ELSE IF (MOD(NODE,2) .EQ. 0) THEN
1001          CALL EIST1(1, NODE)
1002          CALL EIMES(5, 3, NODE = Z(I1) must be an odd integer '///
1003          greater than 4.')
1004      END IF
1005      IF (ALPHA .LE. 0.0) THEN
1006          CALL EIST1(1, ALPHA)
1007          CALL EIMES(5, 4, 'ALPHA = Z(R1); The penalty weighting '///
1008          factor which controls smoothness, ALPHA, must
1009          be greater than 0.')
1010      END IF
1011      IF (MAXIT .LE. 0.0) THEN
1012          CALL EIST1(1, MAXIT)
1013          CALL EIMES(5, 5, MAXIT = Z(I1), The maximum number '///
1014          of iterations, MAXIT, must be greater than 0.')
1015      END IF
1016      IF (ENDS(1) .GT. ENDS(2)) THEN
1017          CALL EIST1(1, ENDS(1))
1018          CALL EIST2(2, ENDS(2))
1019          CALL EIMES(5, 6, 'ENDS(1) = Z(R1) and ENDS(2) = '///
1020          Z(R2). The minimum value for X, BNDS(1), must
1021          be less than or equal to the maximum value for
1022          X, BNDS(2).')
1023      END IF
1024      IF (INIT .NE. 0) THEN
1025          IF (DENS(1) .NE. 0 .OR. DENS(NODE) .NE. 0) THEN
1026              CALL EIST1(1, DENS(1))
1027              CALL EIST2(2, DENS(NODE))
1028              CALL EIST1(1, NODE)
1029              CALL EIMES(5, 7, 'DENS(1) = Z(R1) and DENS(NODE) = Z(I1) '///
1030              = Z(R2). The beginning and ending initial
1031              estimates of the density must be zero.')
1032          END IF
1033          IF (DENS(ISMIN(NODE, DENS(1))) .LT. 0) THEN
1034              IF (CALL EIMES(5, 8, 'The initial estimates of the '///
1035              density, DENS, must be greater than or
1036              equal to 0.'))
1037              END IF
1038          END IF
1039          NOB1 = 0
1040          DO 10 IF (X(1) .LT. ENDS(1) .OR. X(1) .GT. ENDS(2)) THEN
1041              NOB1 = NOB1 + 1
1042          END IF
1043          IF (NOB1 .EQ. NOBS) THEN
1044              10 CONTINUE
1045              IF (CALL EIMES(5, 9, 'All elements in X lie outside the '///
1046              interval, BNDS(1) to BNDS(2). At least one
1047              element of X must lie in this interval.))
1048              END IF
1049          IF (EPS .LE. 0.0) THEN
1050              EPS1 = 1.0E-4
1051          ELSE
1052              EPS1 = EPS
1053          END IF
1054          IF (NIRCD(0) .NE. 0) GO TO 9000
1055      C      IMPTR = 0
1056      C      Initialization
1057      C      IF (INIT .EQ. 0) THEN
1058          DENS(1) = 0.0
1059          DENS(2) = 2.0 / (ENDS(2) - ENDS(1))
1060          DENS(3) = 0.0
1061      END IF

```

```

M = 3
ELSE
M = NODE
END IF

C 20 IF (INIT.EQ. 0) THEN
      Refine mesh
      MOLD = M
      IMPTR = IMPTR + 1
      M = MINO(NODE, MINCR(IMPTR))
      END IF

      Get mesh interval width
      H2 = (BNDS(2) - BNDS(1)) / (M - 1)
      H3 = H2 * H
      END IF

      Make initial DENS integrate to 1.
      IF (INIT.NE. 0) THEN
      CALL SSCAL (NODE, 1.0 / (H * SSUM(NODE, DENS, 1)), DENS, 1)
      END IF

      Set mesh nodes
      B(1) = BNDS(1)
      DO 30 I = 2, M
      B(I) = B(I - 1) + H
      30 CONTINUE

      Set B indices for interpolating X
      IPTR = 0
      IF (X(IPTR) + 1, BNDS(1)) GO TO 40
      DO 60 N = 1, M - 1
      ILOHI(K, 1) = IPTR
      ILOHI(K, 2) = IPTR - 1
      IF (IPTR.LE. NOBS) THEN
      IF (X(IPTR).LT. B(K + 1)) THEN
      ILOHI(K, 2) = ILOHI(K, 2) + 1
      IPTR = IPTR + 1
      IF (IPTR.LE. NOBS) GO TO 50
      END IF
      END IF
      60 CONTINUE
      FACTOR = 2.0 * ALPHA / H3
      IF (INIT.EQ. 0) THEN
      CALL DSPT (M - 2, B(2), 1, MOLD, BNDS, DENS, DENEST, WK, WK,
      &
      TEMP = 1.0 / (M * M * H)
      DO 80 I = 2, M - 1
      DENS(I) = AMAX1(TEMP, SQRT(DENEST(I - 1, 1)))
      80 CONTINUE
      ELSE
      DO 90 I = 2, M - 1
      DENS(I) = SQRT(DENS(I))
      90 CONTINUE
      IF
      DENS(M) = 0.0

      DO 140 ITER = 1, MAXIT
      HESS(1, 1) = 0.0
      HESS(1, 2) = 0.0
      HESS(2, 1) = 0.0
      ESMALL = 0.0
      SUM = 0.0

      CN** are true estimates = FN**2

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DO 120 K=2, M-1
  KM1 = K-1
  KM2 = MAX0(1,K-2)
  KP1 = K+1
  KP2 = MIN0(M,K+2)
  FK = DENSI(K)
  FKMI = DENSI(KM1)
  FKM2 = DENSI(KM2)
  CKM1 = FKM1**2
  CKM2 = FKM2**2
  CK = FKM1**2
  CKP1 = DENSI(KP1)**2
  CKP2 = DENSI(KP2)**2
  BK = B(K)
  BKMI = B(KM1)
  SUM = SUM + CK
  IF (K.GE.4) HESS(1,KM1) = 4.0*FK*FKM2*FACTOR
  SUM1 = 0.0D0
  SUM2 = 0.0D0
  SUM3 = 0.0D0
  DO 100 I=ILOHI(K,1), ILOHI(K,2)
    TEMP = (X(I)-BK)/H
    CONS = (1.0-TEMP)/(CK+(CKP1-CK)*TEMP)
    SUM1 = SUM1 + CONS
    SUM2 = SUM2 + CONS*CONS
    SUM3 = SUM3 + CK - CKM1
    CONTINUE
  CKMCM1 = CK - CKM1
  DO 110 I=ILOHI(KM1,1), ILOHI(KM1,2)
    CONS = (X(I)-BKMI)/H
    TEMP = SUM1 + CKMCM1*CONS
    SUM1 = SUM1 - CONS*TEMP
    SUM2 = TEMP*TEMP
    SUM3 = SUM2 + (CONS*CONS)/TEMP
    CONTINUE
  TEMP = FACTOR*(CKM2+CKP2-4.0*(CKMI+CKP1)+6.0*CK) + SUM1
  RSMALL = 2.0*TEMP
  RSMALL = RSMALL + 2.0*CK*TEMP
  HESS(3,KM1) = TEMP + 4.0*CK*(6.0*FACTOR+SUM2)
  IF (K.NE.2) HESS(2,KM1) = 4.0*FK*FKM1*(-4.0*FACTOR+SUM3)
  DENEST(KM1,1) = FK*TEMP
  DENEST(KM1,2) = -2.0*FK
  CONTINUE
  BSMALL = 1.0/H - SUM + BSMALL
  CALL SCOPY (M-2, DENEST(1,2), 1, DENEST(1,3), 1)
  CALL SADD (M-2, -BSMALL/(2.0*SUM), HESS(3,1), LDHESS)
  CALL SCOPY (M-4, HESS(1,3), LDHESS, HESS(5,1), LDHESS)
  HESS(5,M-3) = 0.0
  HESS(5,M-2) = 0.0
  CALL SCOPY (M-3, HESS(2,2), LDHESS, HESS(4,1), LDHESS)
  HESS(4,M-2) = 0.0
  CALL L2TRB (M-2, HESS, LDHESS, 2, 2, HESS, LDHESS, IPUT, WK2)
  CALL LFSRB (M-2, HESS, LDHESS, 2, 2, IPUT, DENEST, 1, DENEST)
  DENEST(1,2) = 1,
  IF (NIRCD(1).NE.0) GO TO 9000
  CONS = SDOT(M-2,DENEST(1,3),1,DENEST(1,2),1)
  CONS = (1.0/H-SUM-SDOT(M-2,DENEST(1,3),1,DENEST(1,1),1))/CONS
  Update the gradient
  Compute the constant

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```

C      CALL SAXPY (M-2, CONS, DENEST(1,2), 1, DENEST(1,1), 1)
C      Parameter updates
C      CALL SAXPY (M-2, -1.0, DENEST(1,1), 1, DENEST(2), 1)
C      IF (TEMP = SNRM2(M-2,DENEST(2),1), 1, EPS1*TEMP) GO TO 150
C      IF (SNRM2(M-2,DENEST(1),1), EPS1*TEMP) GO TO 150
C      TEMP = TEMP*1.0E-4/SORT(M-2.0)
C      DO 130 I=2, M-1
C      DENEST(I) = AMAX1(TEMP,DENEST(I))
C      130 CONTINUE
C      CALL E1STI (1, MAXIT)
C      CALL E1HES (3, 1, The maximum number of iterations '///
C      IF (MAXIT=2(I1)) was exceeded,
C      150 CALL SHFROD (M-2, DENEST(2), 1, DENEST(2), 1)
C      IF (M.NE. NODE) GO TO 20
C      Evaluate log likelihood and penalty
C      SUM1 = 0.0
C      Penalty
C      DO 160 K=1, M
C      KP1 = MAX0(K-1,1)
C      KP1 = MIN0(K+1,M)
C      SUM1 = SUM1 + (DENS(KM1)-2.0*DENS(K)+DENS(KP1))**2
C      160 CONTINUE
C      SUM2 = -0.5*FACTOR*SUM1
C      SUM2 = 0.0
C      DO 170 I=1, NOBS
C      IF (X(I).GE.BNDS(1) .AND. X(I).LE.BNDS(2)) THEN
C      CALL D2SPT (1, X(I), 1, NODE, BNDS, DENS, DENEST, WK, WK,
C      170 CONTINUE
C      SUM2 = SUM2 + ALOG(DENEST(1,1))
C      END IF
C      Evaluate M.L.F.E. mean and variance
C      SUM1 = 0.0
C      SUM2 = 0.0
C      DO 180 K=1, M-1
C      FK = DENS(K)
C      FKP1 = DENS(K+1)
C      BK = B(K)
C      CONS = FK + FKP1
C      TEMP = CONS + FKP1
C      SUM1 = SUM1 + H2*TEMP/6.0 + 0.5*H*BK*CONS
C      SUM2 = SUM2 + H3*(TEMP+FKP1)/12.0 + H2*BK*TEMP/3.0 +
C      SUM2 = 0.5*H*BK*BK*CONS
C      180 CONTINUE
C      STAT(3) = SUM1
C      STAT(4) = SUM2 - SUM1*SUM1
C      9000 CALL E1POP ('D3SPL ')
C      RETURN
C      END
/EOF

```


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1
28.0E-01
300.0E-06
2.20E-11
6.2E+02
21
40
1.4E-01
45.0E-06
0.23E-11
6.3E+01
50.0E-01
10.0E-05 30
22

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```
21 0 0.5000E+01 0.1000E-03 30
NDS(1),ENDS(2)= 0.2724E+01 0.5153E+01
DF OF LOG OF CURRENT CYCLES, LOG XNF, Y AXIS OF PDF PLOT
0.0000E+00 0.3049E-01 0.1355E+00 0.2417E+00 0.3572E+00
0.4706E+00 0.5719E+00 0.6542E+00 0.7124E+00 0.7426E+00
0.7450E+00 0.7193E+00 0.6884E+00 0.5957E+00 0.5065E+00
0.4067E+00 0.3027E+00 0.2019E+00 0.1118E+00 0.4101E-01
OUTPUT STATISTICS
-0.2267E+02 -0.1434E+02 0.3913E+01 0.2274E+00
NUMBER OF MISSING VALUES
LOG OF CURRENT CYCLES, LOG XNF
0.3210E+01 0.3849E+01 0.3533E+01 0.3267E+01 0.3089E+01
0.3810E+01 0.3332E+01 0.3453E+01 0.3574E+01 0.3696E+01
0.4421E+01 0.3939E+01 0.4080E+01 0.4182E+01 0.4303E+01
0.4546E+01 0.4667E+01 0.4789E+01 0.4910E+01 0.5031E+01
ORDERED LOG OF CURRENT CYCLES, LOG XNF, X AXIS PDF, CDF PLOT
0.2724E+01 0.2846E+01 0.2967E+01 0.3089E+01 0.3210E+01
0.3332E+01 0.3453E+01 0.3574E+01 0.3696E+01 0.3817E+01
0.3939E+01 0.4060E+01 0.4182E+01 0.4303E+01 0.4424E+01
0.4544E+01 0.4667E+01 0.4789E+01 0.4910E+01 0.5031E+01
GDF PARAMETERS
CDF OF LOG OF CURRENT CYCLES, LOG XNF, Y AXIS OF PDF, CDF PLOT
0.0000E+00 0.3065E-02 0.1435E-01 0.3725E-01 0.7362E-01
0.1239E+00 0.1872E+00 0.2616E+00 0.3446E+00 0.4329E+00
0.5232E+00 0.6121E+00 0.6984E+00 0.7731E+00 0.8400E+00
0.8955E+00 0.9385E+00 0.9692E+00 0.9882E+00 0.9975E+00
ORDERED LOG OF CURRENT CYCLES, LOG XNF, X AXIS OF PDF, CDF PLOT
0.2724E+01 0.2846E+01 0.2967E+01 0.3089E+01 0.3210E+01
0.3332E+01 0.3453E+01 0.3574E+01 0.3696E+01 0.3817E+01
0.3939E+01 0.4060E+01 0.4182E+01 0.4303E+01 0.4424E+01
0.4544E+01 0.4667E+01 0.4789E+01 0.4910E+01 0.5031E+01
0.5153E+01 0.5274E+01 0.5395E+01 0.5516E+01 0.5637E+01
0.5758E+01 0.5879E+01 0.5999E+01 0.6120E+01 0.6241E+01
0.6362E+01 0.6483E+01 0.6604E+01 0.6725E+01 0.6846E+01
0.6967E+01 0.7088E+01 0.7209E+01 0.7330E+01 0.7451E+01
0.7572E+01 0.7693E+01 0.7814E+01 0.7935E+01 0.8056E+01
0.8177E+01 0.8298E+01 0.8419E+01 0.8540E+01 0.8661E+01
0.8782E+01 0.8903E+01 0.9024E+01 0.9145E+01 0.9266E+01
0.9387E+01 0.9508E+01 0.9629E+01 0.9750E+01 0.9871E+01
0.9992E+01 1.0113E+01 1.0234E+01 1.0355E+01 1.0476E+01
1.0597E+01 1.0718E+01 1.0839E+01 1.0960E+01 1.1081E+01
1.1202E+01 1.1323E+01 1.1444E+01 1.1565E+01 1.1686E+01
1.1807E+01 1.1928E+01 1.2049E+01 1.2170E+01 1.2291E+01
1.2412E+01 1.2533E+01 1.2654E+01 1.2775E+01 1.2896E+01
1.3017E+01 1.3138E+01 1.3259E+01 1.3380E+01 1.3501E+01
1.3622E+01 1.3743E+01 1.3864E+01 1.3985E+01 1.4106E+01
1.4227E+01 1.4348E+01 1.4469E+01 1.4590E+01 1.4711E+01
1.4832E+01 1.4953E+01 1.5074E+01 1.5195E+01 1.5316E+01
1.5437E+01 1.5558E+01 1.5679E+01 1.5800E+01 1.5921E+01
1.6042E+01 1.6163E+01 1.6284E+01 1.6405E+01 1.6526E+01
1.6647E+01 1.6768E+01 1.6889E+01 1.7010E+01 1.7131E+01
1.7252E+01 1.7373E+01 1.7494E+01 1.7615E+01 1.7736E+01
1.7857E+01 1.7978E+01 1.8099E+01 1.8220E+01 1.8341E+01
1.8462E+01 1.8583E+01 1.8704E+01 1.8825E+01 1.8946E+01
1.9067E+01 1.9188E+01 1.9309E+01 1.9430E+01 1.9551E+01
1.9672E+01 1.9793E+01 1.9914E+01 2.0035E+01 2.0156E+01
2.0277E+01 2.0398E+01 2.0519E+01 2.0640E+01 2.0761E+01
2.0882E+01 2.1003E+01 2.1124E+01 2.1245E+01 2.1366E+01
2.1487E+01 2.1608E+01 2.1729E+01 2.1850E+01 2.1971E+01
2.2092E+01 2.2213E+01 2.2334E+01 2.2455E+01 2.2576E+01
2.2697E+01 2.2818E+01 2.2939E+01 2.3060E+01 2.3181E+01
2.3302E+01 2.3423E+01 2.3544E+01 2.3665E+01 2.3786E+01
2.3907E+01 2.4028E+01 2.4149E+01 2.4270E+01 2.4391E+01
2.4512E+01 2.4633E+01 2.4754E+01 2.4875E+01 2.4996E+01
2.5117E+01 2.5238E+01 2.5359E+01 2.5480E+01 2.5601E+01
2.5722E+01 2.5843E+01 2.5964E+01 2.6085E+01 2.6206E+01
2.6327E+01 2.6448E+01 2.6569E+01 2.6690E+01 2.6811E+01
2.6932E+01 2.7053E+01 2.7174E+01 2.7295E+01 2.7416E+01
2.7537E+01 2.7658E+01 2.7779E+01 2.7900E+01 2.8021E+01
2.8142E+01 2.8263E+01 2.8384E+01 2.8505E+01 2.8626E+01
2.8747E+01 2.8868E+01 2.8989E+01 2.9110E+01 2.9231E+01
2.9352E+01 2.9473E+01 2.9594E+01 2.9715E+01 2.9836E+01
2.9957E+01 3.0078E+01 3.0199E+01 3.0320E+01 3.0441E+01
3.0562E+01 3.0683E+01 3.0804E+01 3.0925E+01 3.1046E+01
3.1167E+01 3.1288E+01 3.1409E+01 3.1530E+01 3.1651E+01
3.1772E+01 3.1893E+01 3.2014E+01 3.2135E+01 3.2256E+01
3.2377E+01 3.2498E+01 3.2619E+01 3.2740E+01 3.2861E+01
3.2982E+01 3.3103E+01 3.3224E+01 3.3345E+01 3.3466E+01
3.3587E+01 3.3708E+01 3.3829E+01 3.3950E+01 3.4071E+01
3.4192E+01 3.4313E+01 3.4434E+01 3.4555E+01 3.4676E+01
3.4797E+01 3.4918E+01 3.5039E+01 3.5160E+01 3.5281E+01
3.5402E+01 3.5523E+01 3.5644E+01 3.5765E+01 3.5886E+01
3.6007E+01 3.6128E+01 3.6249E+01 3.6370E+01 3.6491E+01
3.6612E+01 3.6733E+01 3.6854E+01 3.6975E+01 3.7096E+01
3.7217E+01 3.7338E+01 3.7459E+01 3.7580E+01 3.7701E+01
3.7822E+01 3.7943E+01 3.8064E+01 3.8185E+01 3.8306E+01
3.8427E+01 3.8548E+01 3.8669E+01 3.8790E+01 3.8911E+01
3.9032E+01 3.9153E+01 3.9274E+01 3.9395E+01 3.9516E+01
3.9637E+01 3.9758E+01 3.9879E+01 4.0000E+01 4.0121E+01
4.0242E+01 4.0363E+01 4.0484E+01 4.0605E+01 4.0726E+01
4.0847E+01 4.0968E+01 4.1089E+01 4.1210E+01 4.1331E+01
4.1452E+01 4.1573E+01 4.1694E+01 4.1815E+01 4.1936E+01
4.2057E+01 4.2178E+01 4.2299E+01 4.2420E+01 4.2541E+01
4.2662E+01 4.2783E+01 4.2904E+01 4.3025E+01 4.3146E+01
4.3267E+01 4.3388E+01 4.3509E+01 4.3630E+01 4.3751E+01
4.3872E+01 4.3993E+01 4.4114E+01 4.4235E+01 4.4356E+01
4.4477E+01 4.4598E+01 4.4719E+01 4.4840E+01 4.4961E+01
4.5082E+01 4.5203E+01 4.5324E+01 4.5445E+01 4.5566E+01
4.5687E+01 4.5808E+01 4.5929E+01 4.6050E+01 4.6171E+01
4.6292E+01 4.6413E+01 4.6534E+01 4.6655E+01 4.6776E+01
4.6897E+01 4.7018E+01 4.7139E+01 4.7260E+01 4.7381E+01
4.7502E+01 4.7623E+01 4.7744E+01 4.7865E+01 4.7986E+01
4.8107E+01 4.8228E+01 4.8349E+01 4.8470E+01 4.8591E+01
4.8712E+01 4.8833E+01 4.8954E+01 4.9075E+01 4.9196E+01
4.9317E+01 4.9438E+01 4.9559E+01 4.9680E+01 4.9801E+01
4.9922E+01 5.0043E+01 5.0164E+01 5.0285E+01 5.0406E+01
5.0527E+01 5.0648E+01 5.0769E+01 5.0890E+01 5.1011E+01
5.1132E+01 5.1253E+01 5.1374E+01 5.1495E+01 5.1616E+01
5.1737E+01 5.1858E+01 5.1979E+01 5.2100E+01 5.2221E+01
5.2342E+01 5.2463E+01 5.2584E+01 5.2705E+01 5.2826E+01
5.2947E+01 5.3068E+01 5.3189E+01 5.3310E+01 5.3431E+01
5.3552E+01 5.3673E+01 5.3794E+01 5.3915E+01 5.4036E+01
5.4157E+01 5.4278E+01 5.4399E+01 5.4520E+01 5.4641E+01
5.4762E+01 5.4883E+01 5.5004E+01 5.5125E+01 5.5246E+01
5.5367E+01 5.5488E+01 5.5609E+01 5.5730E+01 5.5851E+01
5.5972E+01 5.6093E+01 5.6214E+01 5.6335E+01 5.6456E+01
5.6577E+01 5.6698E+01 5.6819E+01 5.6940E+01 5.7061E+01
5.7182E+01 5.7303E+01 5.7424E+01 5.7545E+01 5.7666E+01
5.7787E+01 5.7908E+01 5.8029E+01 5.8150E+01 5.8271E+01
5.8392E+01 5.8513E+01 5.8634E+01 5.8755E+01 5.8876E+01
5.8997E+01 5.9118E+01 5.9239E+01 5.9360E+01 5.9481E+01
5.9602E+01 5.9723E+01 5.9844E+01 5.9965E+01 6.0086E+01
6.0207E+01 6.0328E+01 6.0449E+01 6.0570E+01 6.0691E+01
6.0812E+01 6.0933E+01 6.1054E+01 6.1175E+01 6.1296E+01
6.1417E+01 6.1538E+01 6.1659E+01 6.1780E+01 6.1901E+01
6.2022E+01 6.2143E+01 6.2264E+01 6.2385E+01 6.2506E+01
6.2627E+01 6.2748E+01 6.2869E+01 6.2990E+01 6.3111E+01
6.3232E+01 6.3353E+01 6.3474E+01 6.3595E+01 6.3716E+01
6.3837E+01 6.3958E+01 6.4079E+01 6.4200E+01 6.4321E+01
6.4442E+01 6.4563E+01 6.4684E+01 6.4805E+01 6.4926E+01
6.5047E+01 6.5168E+01 6.5289E+01 6.5410E+01 6.5531E+01
6.5652E+01 6.5773E+01 6.5894E+01 6.6015E+01 6.6136E+01
6.6257E+01 6.6378E+01 6.6499E+01 6.6620E+01 6.6741E+01
6.6862E+01 6.6983E+01 6.7104E+01 6.7225E+01 6.7346E+01
6.7467E+01 6.7588E+01 6.7709E+01 6.7830E+01 6.7951E+01
6.8072E+01 6.8193E+01 6.8314E+01 6.8435E+01 6.8556E+01
6.8677E+01 6.8798E+01 6.8919E+01 6.9040E+01 6.9161E+01
6.9282E+01 6.9403E+01 6.9524E+01 6.9645E+01 6.9766E+01
6.9887E+01 7.0008E+01 7.0129E+01 7.0250E+01 7.0371E+01
7.0492E+01 7.0613E+01 7.0734E+01 7.0855E+01 7.0976E+01
7.1097E+01 7.1218E+01 7.1339E+01 7.1460E+01 7.1581E+01
7.1702E+01 7.1823E+01 7.1944E+01 7.2065E+01 7.2186E+01
7.2307E+01 7.2428E+01 7.2549E+01 7.2670E+01 7.2791E+01
7.2912E+01 7.3033E+01 7.3154E+01 7.3275E+01 7.3396E+01
7.3517E+01 7.3638E+01 7.3759E+01 7.3880E+01 7.4001E+01
7.4122E+01 7.4243E+01 7.4364E+01 7.4485E+01 7.4606E+01
7.4727E+01 7.4848E+01 7.4969E+01 7.5090E+01 7.5211E+01
7.5332E+01 7.5453E+01 7.5574E+01 7.5695E+01 7.5816E+01
7.5937E+01 7.6058E+01 7.6179E+01 7.6300E+01 7.6421E+01
7.6542E+01 7.6663E+01 7.6784E+01 7.6905E+01 7.7026E+01
7.7147E+01 7.7268E+01 7.7389E+01 7.7510E+01 7.7631E+01
7.7752E+01 7.7873E+01 7.7994E+01 7.8115E+01 7.8236E+01
7.8357E+01 7.8478E+01 7.8599E+01 7.8720E+01 7.8841E+01
7.8962E+01 7.9083E+01 7.9204E+01 7.9325E+01 7.9446E+01
7.9567E+01 7.9688E+01 7.9809E+01 7.9930E+01 8.0051E+01
8.0172E+01 8.0293E+01 8.0414E+01 8.0535E+01 8.0656E+01
8.0777E+01 8.0898E+01 8.1019E+01 8.1140E+01 8.1261E+01
8.1382E+01 8.1503E+01 8.1624E+01 8.1745E+01 8.1866E+01
8.1987E+01 8.2108E+01 8.2229E+01 8.2350E+01 8.2471E+01
8.2592E+01 8.2713E+01 8.2834E+01 8.2955E+01 8.3076E+01
8.3197E+01 8.3318E+01 8.3439E+01 8.3560E+01 8.3681E+01
8.3802E+01 8.3923E+01 8.4044E+01 8.4165E+01 8.4286E+01
8.4407E+01 8.4528E+01 8.4649E+01 8.4770E+01 8.4891E+01
8.5012E+01 8.5133E+01 8.5254E+01 8.5375E+01 8.5496E+01
8.5617E+01 8.5738E+01 8.5859E+01 8.5980E+01 8.6101E+01
8.6222E+01 8.6343E+01 8.6464E+01 8.6585E+01 8.6706E+01
8.6827E+01 8.6948E+01 8.7069E+01 8.7190E+01 8.7311E+01
8.7432E+01 8.7553E+01 8.7674E+01 8.7795E+01 8.7916E+01
8.8037E+01 8.8158E+01 8.8279E+01 8.8400E+01 8.8521E+01
8.8642E+01 8.8763E+01 8.8884E+01 8.9005E+01 8.9126E+01
8.9247E+01 8.9368E+01 8.9489E+01 8.9610E+01 8.9731E+01
8.9852E+01 8.9973E+01 9.0094E+01 9.0215E+01 9.0336E+01
9.0457E+01 9.0578E+01 9.0699E+01 9.0820E+01 9.0941E+01
9.1062E+01 9.1183E+01 9.1304E+01 9.1425E+01 9.1546E+01
9.1667E+01 9.1788E+01 9.1909E+01 9.2030E+01 9.2151E+01
9.2272E+01 9.2393E+01 9.2514E+01 9.2635E+01 9.2756E+01
9.2877E+01 9.2998E+01 9.3119E+01 9.3240E+01 9.3361E+01
9.3482E+01 9.3603E+01 9.3724E+01 9.3845E+01 9.3966E+01
9.4087E+01 9.4208E+01 9.4329E+01 9.4450E+01 9.4571E+01
9.4692E+01 9.4813E+01 9.4934E+01 9.5055E+01 9.5176E+01
9.5297E+01 9.5418E+01 9.5539E+01 9.5660E+01 9.5781E+01
9.5902E+01 9.6023E+01 9.6144E+01 9.6265E+01 9.6386E+01
9.6507E+01 9.6628E+01 9.6749E+01 9.6870E+01 9.6991E+01
9.7112E+01 9.7233E+01 9.7354E+01 9.7475E+01 9.7596E+01
9.7717E+01 9.7838E+01 9.7959E+01 9.8080E+01 9.8201E+01
9.8322E+01 9.8443E+01 9.8564E+01 9.8685E+01 9.8806E+01
9.8927E+01 9.9048E+01 9.9169E+01 9.9290E+01 9.9411E+01
9.9532E+01 9.9653E+01 9.9774E+01 9.9895E+01 1.0016E+02
1.0137E+02 1.0258E+02 1.0379E+02 1.0500E+02 1.0621E+02
1.0742E+02 1.0863E+02 1.0984E+02 1.1105E+02 1.1226E+02
1.1347E+02 1.1468E+02 1.1589E+02 1.1710E+02 1.1831E+02
1.1952E+02 1.2073E+02 1.2194E+02 1.2315E+02 1.2436E+02
1.2557E+02 1.2678E+02 1.2799E+02 1.2920E+02 1.3041E+02
1.3162E+02 1.3283E+02 1.3404E+02 1.3525E+02 1.3646E+02
1.3767E+02 1.3888E+02 1.4009E+02 1.4130E+02 1.4251E+02
1.4372E+02 1.4493E+02 1.4614E+02 1.4735E+02 1.4856E+02
1.4977E+02 1.5098E+02 1.5219E+02 1.5340E+02 1.5461E+02
1.5582E+02 1.5703E+02 1.5824E+02 1.5945E+02 1.6066E+02
1.6187E+02 1.6308E+02 1.6429E+02 1.6550E+02 1.6671E+02
1.6792E+02 1.6913E+02 1.7034E+02 1.7155E+02 1.7276E+02
1.7397E+02 1.7518E+02 1.7639E+02 1.7760E+02 1.7881E+02
1.8002E+02 1.8123E+02 1.8244E+02 1.8365E+02 1.8486E+02
1.8607E+02 1.8728E+02 1.8849E+02 1.8970E+02 1.9091E+02
1.9212E+02 1.9333E+02 1.9454E+02 1.9575E+02 1.9696E+02
1.9817E+02 1.9938E+02 2.0059E+02 2.0180E+02 2.0301E+02
2.0422E+02 2.0543E+02 2.0664E+02 2.0785E+02 2.0906E+02
2.1027E+02 2.1148E+02 2.1269E+02 2.1390E+02 2.1511E+02
2.1632E+02 2.1753E+02 2.1874E+02 2.1995E+02 2.2116E+02
2.2237E+02 2.2358E+02 2.2479E+02 2.2600E+02 2.2721E+02
2.2842E+02 2.2963E+02 2.3084E+02 2.3205E+02 2.3326E+02
2.3447E+02 2.3568E+02 2.3689E+02 2.3810E+02 2.3931E+02
2.4052E+02 2.4173E+02 2.4294E+02 2.4415E+02 2.4536E+02
2.4657E+02 2.4778E+02 2.4899E+02 2.5020E+02 2.5141E+02
2.5262E+02 2.5383E+02 2.5504E+02 2.5625E+02 2.5746E+02
2.5867E+02 2.5988E+02 2.6109E+02 2.6230E+02 2.6351E+02
2.6472E+02 2.6593E+02 2.6714E+02 2.6835E+02 2.6956E+02
2.7077E+02 2.7198E+02 2.7319E+02 2.7440E+02 2.7561E+02
2.7682E+02 2.7803E+02 2.7924E+02 2.8045E+02 2.8166E+02
2.8287E+02 2.8408E+02 2.8529E+02 2.8650E+02 2.8771E+02
2.8892E+02 2.9013E+02 2.9134E+02 2.9255E+02 2.9376E+02
2.9497E+02 2.9618E+02 2.9739E+02 2.9860E+02 2.9981E+02
3.0102E+02 3.0223E+02 3.0344E+02 3.0465E+02 3.0586E+02
3.0707E+02 3.0828E+02 3.0949E+02 3.1070E+02 3.1191E+02
3.1312E+02 3.1433E+02 3.1554E+02 3.1675E+02 3.1796E+02
3.1917E+02 3.2038E+02 3.2159E+02 3.2280E+02 3.2401E+02
3.2522E+02 3.2643E+02 3.2764E+02 3.2885E+02 3.3006E+02
3.3127E+02 3.3248E+02 3.3369E+02 3.3490E+02 3.3611E+02
3.3732E+02 3.3853E+02 3.3974E+02 3.4095E+02 3.4216E+02
3.4337E+02 3.4458E+02 3.4579E+02 3.4700E+02 3.4821E+02
3.4942E+02 3.5063E+02 3.5184E+02 3.5305E+02 3.5426E+02
3.5547E+02 3.5668E+02 3.5789E+02 3.5910E+02 3.603
```

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27 0

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ORIGINAL PAGE IS
OF POOR QUALITY

TIME	USER	SECTORS	TEMPORARY DATASET SECTORS USED	PERMANENT DATASET SECTORS USED	SECTORS QUEUED TO FRONT END	RT seconds	RT seconds	RT seconds
11:18:03.1152	USER	7.6744	7.6742 CPU seconds	5.7557 RT seconds	82%			
11:18:03.1153	USER	7.6744	467 I/O requests	0.1401 RT seconds	2%			
11:18:03.1154	USER	7.6744	1.7996 CHCPU mwdsec	0.5399 RT seconds	8%			
11:18:03.1155	USER	7.6744	1.8168 CHXIO requests	0.5450 RT seconds	8%			
11:18:03.1156	USER	7.6744						
11:18:03.1157	USER	7.6744						
11:18:03.1158	USER	7.6744						
11:18:03.1159	USER	7.6744						
11:18:03.1160	USER	7.6744						
11:18:03.1161	USER	7.6744						
11:18:03.1162	USER	7.6744						
11:18:03.1163	USER	7.6744						
11:18:03.1164	USER	7.6744						
11:18:03.1165	USER	7.6744						
11:18:03.1166	USER	7.6744						
11:18:03.1167	USER	7.6744						
11:18:03.1168	USER	7.6744						
11:18:03.1169	USER	7.6744						
11:18:03.1170	USER	7.6744						
11:18:03.1171	USER	7.6744						
11:18:03.1172	USER	7.6744						
11:18:03.1173	USER	7.6744						
11:18:03.1174	USER	7.6744						
11:18:03.1175	USER	7.6744						
11:18:03.1176	USER	7.6744						
11:18:03.1177	USER	7.6744						
11:18:03.1178	USER	7.6744						
11:18:03.1179	USER	7.6744						
11:18:03.1180	USER	7.6744						
11:18:03.1181	USER	7.6744						
11:18:03.1182	USER	7.6744						
11:18:03.1183	USER	7.6744						
11:18:03.1184	USER	7.6744						
11:18:03.1185	USER	7.6744						
11:18:03.1186	USER	7.6744						
11:18:03.1187	USER	7.6744						
11:18:03.1188	USER	7.6744						
11:18:03.1189	USER	7.6744						
11:18:03.1190	USER	7.6744						
11:18:03.1191	USER	7.6744						
11:18:03.1192	USER	7.6744						
Total				6.9807 RT seconds				
RT cost at bid priority 2				\$	0.97			

A 10x10 grid of 100 squares, each containing a number from 1 to 100 in a random order. The numbers are arranged in a way that suggests a specific pattern or sequence, but the exact details are obscured by the low resolution of the image.

Y Y Y
Y Y Y
Y Y Y

[illegible]

8.0 APPENDIX C

IMSL SUBROUTINE CALLS FROM RANDOM2

1. RNSET - Initializes a random seed for use in the IMSL random number generators.
2. RNNOR - Generates pseudorandom numbers from a standard normal distribution using an inverse CDF method.
3. RNLNL - Generates pseudorandom numbers from a lognormal distribution.
4. DESPL - Performs nonparametric probability density function estimation by the penalized likelihood method.
5. GCDF - Evaluates a general continuous cumulative distribution function given ordinates of the density.

9.0 APPENDIX D

SAMPLE SAS/GRAPH (VER. 5.16) PROGRAM FOR RANDOM2

```
data a;
INFILE 'OUT1.CPR' FIRSTOBS=2;input x y;
GOPTIONS DEVICE=HP7470;
proc gplot;
  axis1 label=(h=1 f=simplex 'LOG OF CYCLES')
        value=(h=1 f=simplex);
  axis2 value=(h=1 f=simplex) label=none;
  plot y*x / haxis=axis1 vaxis=axis2;
  TITLE H=1 A=90 F=SIMPLEX 'PROBABILITY DENSITY FUNCTION';
  symbol i=spline v=square;
data B;
INFILE 'OUT2.CPR' FIRSTOBS=2;input x y;
proc gplot;
  axis1 label=(h=1 f=simplex 'LOG OF CYCLES')
        value=(h=1 f=simplex);
  axis2 value=(h=1 f=simplex) label=none;
  plot y*x / haxis=axis1 vaxis=axis2;
  TITLE H=1 A=90 F=SIMPLEX 'CUMULATIVE DISTRIBUTION FUNCTION';
  symbol i=spline v=square;
```